

Name: Logan Roberts

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Problem Set Number: #4

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Acknowledgement:

No help

# 1 Known:

- $L_g = 3 \text{ mm} = .003 \text{ m}$ ,  $k_g = 1.5 \text{ W/(mK)}$
- $L_a = .1 \text{ mm} = 1 \times 10^{-4} \text{ m}$ ,  $k_a = 1 \text{ W/(mK)}$
- $R_c = 10^{-4} \text{ m}^2 \text{K/W}$
- $C = 800 \text{ W/m}^2$
- $T_{\infty} = T_{\text{amb}} = 300 \text{ K}$
- $h = 10 \text{ W/(m}^2 \text{K)}$
- $h_{\text{rad}} = 5 \text{ W/(m}^2 \text{K)}$
- $a = .553$   $b = .001 \text{ K}^{-1}$

# Find:

- A) Thermal resistance + assumptions + each resistance value
- B)  $T_{g, \text{top}}$ ,  $T_{Si}$
- C)  $\eta$  and electric power flux  $q_{\text{elec}}$

# Assumptions:

1. Steady state
2. 1-D conduction through layers, uniform properties
3. Silicon is "very thin"  $\rightarrow$  represented by a node at  $T_{Si}$
4. Backside insulated  $\rightarrow$  no heat loss from backside, all heat leaves the top surface.
5. Radiation modeled via effective coefficient  $h_{\text{rad}}$

# A

$$R_g = \frac{L_g}{k_g} = \frac{.003}{1.5} = 2 \times 10^{-3}$$

$$R_a = \frac{L_a}{k_a} = \frac{1 \times 10^{-4}}{1} = 1 \times 10^{-4}$$

Series conduction from silicon to top surface

$$R_{\text{cond}} = R_c + R_a + R_g = .0001 + .0001 + .0020 = 2.2 \times 10^{-3}$$

Top surface heat loss:

$$h_{\text{tot}} = h + h_{\text{rad}} = 10 + 5 = 15 \text{ W/(m}^2 \text{K)} \rightarrow R_{\text{surf}} = \frac{1}{h_{\text{tot}}} = \frac{1}{15} = 6.67 \times 10^{-2}$$

$$R_g = 2 \times 10^{-3}, R_a = 1 \times 10^{-4}, R_c = 1 \times 10^{-4}, R_{\text{cond}} = 2.2 \times 10^{-3}, R_{\text{surf}} = 6.67 \times 10^{-2}$$

# B

Solar at glass top:

$$q_{g, \text{abs}} = .1G = .1(800) = 80 \text{ W/m}^2$$

Solar Silicon:

$$q_{Si, \text{abs}} = .85G = .85(800) = 680 \text{ W/m}^2$$

Electrical conversion:

$$\eta = a - bT_{Si} = .553 - .001T_{Si}$$

Thermal generated in silicon:

$$q_{Si, \text{th}} = (1 - \eta)q_{Si, \text{abs}}$$

Total heat that must leave from the top surface:

$$q = q_{g, \text{abs}} + q_{Si, \text{th}} = 80 + (1 - \eta)680$$

Top surface energy balance:

$$q = h_{\text{tot}}(T_{g, \text{top}} - T_{\infty}) \Rightarrow T_{g, \text{top}} = T_{\infty} + \frac{q}{h_{\text{tot}}}$$

Conduction from silicon to top surface:

$$q = h_{\text{tot}}(T_{g, \text{top}} - T_{\infty}) \Rightarrow T_{g, \text{top}} = T_{\infty} + \frac{q}{h_{\text{tot}}}$$

Conduction from silicon to top surface:

$$T_{Si} = T_{g, \text{top}} + qR_{\text{cond}}$$

$$T_{Si} = 342.48 \text{ K} \quad T_{g, \text{top}} = 341.12 \text{ K}$$

# C

$$\eta = .553 - .001(342.48) = .2105$$

$$q_{\text{elec}} = \eta q_{Si, \text{abs}} = .2105(680) = 143.15 \text{ W/m}^2$$

$$\eta = .2105 (\approx 21.1\%) \quad q_{\text{elec}} = 143.15 \text{ W/m}^2$$

2

Known:

- $D = 10 \text{ mm} = .01 \text{ m}$ ,  $k = 80 \text{ W/(mK)}$
- Wall temp:  $T_w = 200^\circ \text{C}$
- Insulation thickness:  $L_{\text{ins}} = 200 \text{ mm} = .2 \text{ m}$
- Ambient:  $T_\infty = 20^\circ \text{C}$ ,  $h = 20 \text{ W/(m}^2\text{K)}$
- Tip insulated

Find:

- A)  $T_0(L_0)$  expression
- B)  $T_0$  for  $L_0 = .2 \text{ m}$  + check  $T_{\text{max}} = 100^\circ \text{C}$
- C) Min.  $L_0$  for  $T_0 \leq 100^\circ \text{C}$

Assumptions:

1. Steady state, 1D conduction along rod in insulated region.
2. Exposed portion behaves as a straight fin with adiabatic tip
3. Constant  $k$ , uniform  $h$ .

A

$$A = \frac{\pi D^2}{4}, P = \pi D$$

$$m = \sqrt{\frac{hP}{kA}}$$

$$q = \frac{kA}{L_{\text{ins}}}(T_w - T_0) \rightarrow q = \sqrt{hPkA}(T_w - T_0)$$

$$C = L_{\text{ins}} m \tanh(mL_0)$$

$$T_0 = \frac{T_w + CT}{1+C} \rightarrow T_0(L_0) = \frac{T_w + (L_{\text{ins}} m \tanh(mL_0)) T_\infty}{1 + L_{\text{ins}} m \tanh(mL_0)}$$

B

$$L_0 = .2 \text{ m}$$

$$m = \sqrt{\frac{hP}{kA}} = \sqrt{\frac{h(4/D)}{k}} = \sqrt{\frac{4h}{kD}} = \sqrt{\frac{4(20)}{80(0.01)}} = 10$$

$$C = L_{\text{ins}} m \tanh(mL_0) = .2(10) \tanh(10 \cdot .2) = 2 \tanh(2) = 1.928$$

$$T_0 = \frac{200 + 1.928(20)}{1 + 1.928} = 81.45^\circ \text{C}$$

$$T_0 = 81.45^\circ \text{C} \rightarrow T_0 < T_{\text{max}} = 100^\circ \text{C} \text{ meets limit}$$

C

$$T_0 = 100^\circ \text{C}$$

$$T_0 = \frac{T_w + CT}{1+C} \rightarrow C = \frac{T_0 - T_w}{T_\infty - T_0} = \frac{100 - 200}{20 - 100} = 1.25$$

$$C = L_{\text{ins}} m \tanh(mL_0) = .2(10) \tanh(10L_0) = 2 \tanh(10L_0)$$

$$2 \tanh(10L_0) = 1.25 \rightarrow \tanh(10L_0) = .625$$

$$10L_0 = \text{arctanh}(.625) = .73317 \rightarrow L_0 = .07332$$

$$L_{0,\text{min}} = .0733 \text{ m } (\approx 73.3 \text{ mm})$$

3

Known:

- Copper fin:  $k = 400 \text{ W/(mK)}$
- Square width:  $s = 10 \text{ mm} = 0.01 \text{ m}$
- $h = 100 \text{ W/(m}^2\text{K)}$
- $\eta_f = 0.6$
- Convection tip

Find:

- A) Fin length  $L$
- B) Fin thermal resistance  $R_f$  and fin effectiveness  $\epsilon_f$

Assumptions:

1. Straight fin, uniform cross-section, constant  $k$ , uniform  $h$ .
2. Use corrected length method for convection tip:  $L_c = L + \frac{A_c}{P}$

Geometry and fin parameter

$$A_c = s^2 = (0.01)^2 = 1 \times 10^{-4} \text{ m}^2$$

$$P = 4s = 4(0.01) = 0.04 \text{ m}$$

$$m = \sqrt{\frac{hP}{kA_c}} = \sqrt{\frac{100(0.04)}{400(10^{-4})}} = 10 \text{ m}^{-1}$$

Corrected Length:

$$L_c = L + \frac{A_c}{P} = L + \frac{10^{-4}}{0.04} = L + 0.0025$$

A

$$\eta_f = \frac{\tanh(mL_c)}{mL_c} = 0.6$$

$$x = mL_c$$

$$\tanh(x)/x = 0.6 \Rightarrow x = 1.51222$$

$$L_c = \frac{x}{m} = \frac{1.51222}{10} = 0.151222 \text{ m}$$

$$L = L_c - \frac{A_c}{P} = 0.151222 - 0.0025 = 0.148722 \text{ m}$$

$$L \approx 149 \text{ mm}$$

B

$$A_f = PL + A_c = (0.04)(0.148722) + 10^{-4} = 0.0060489 \text{ m}^2$$

$$Q_f = \eta_f h A_f (T_b - T_\infty) \rightarrow R_f = \frac{T_b - T_\infty}{Q_f} = \frac{1}{\eta_f h A_f}$$

$$R_f = \frac{1}{(0.6)(100)(0.0060489)} = 2.755 \text{ K/W}$$

$$\epsilon_f = \frac{Q_f}{h A_c (T_b - T_\infty)} = \eta_f \frac{A_f}{A_c} = 0.6 \frac{0.0060489}{10^{-4}} = 36.29$$

$$R_f = 2.76 \text{ K/W} \quad \epsilon_f = 36.3$$